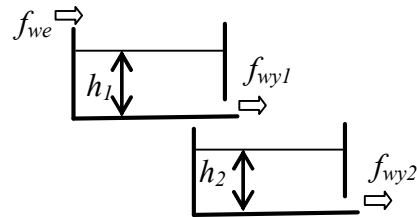


## Otwarte układy hydrauliczne (modele dokładne)

### Kaskada niewspółdziałająca



$$\begin{cases} A_1 \dot{h}_1(t) = f_{we}(t) - f_{wy1}(t) \\ A_2 \dot{h}_2(t) = f_{wy1}(t) - f_{wy2}(t) \end{cases}$$

$$f_{wy1}(t) = A_{w1} \sqrt{2gh_1(t)}$$

$$f_{wy2}(t) = A_{w2} \sqrt{2gh_2(t)}$$

$$\begin{cases} A_1 \dot{h}_1(t) = f_{we}(t) - A_{w1} \sqrt{2gh_1(t)} \\ A_2 \dot{h}_2(t) = A_{w1} \sqrt{2gh_1(t)} - A_{w2} \sqrt{2gh_2(t)} \end{cases}$$

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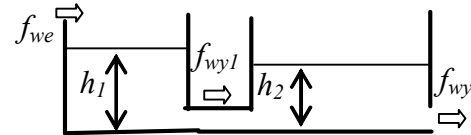

$$\begin{cases} 0 = f_{we} - A_{w1} \sqrt{2gh_1} \\ 0 = A_{w1} \sqrt{2gh_1} - A_{w2} \sqrt{2gh_2} \end{cases}$$

$$f_{we} = A_{w1} \sqrt{2gh_1} = A_{w2} \sqrt{2gh_2}$$

$$h_1 =$$

$$h_2 =$$

### Kaskada współdziałająca



$$\begin{cases} A_1 \dot{h}_1(t) = f_{we}(t) - f_{wy1}(t) \\ A_2 \dot{h}_2(t) = f_{wy1}(t) - f_{wy2}(t) \end{cases}$$

$$f_{wy1}(t) = A_{w1} \sqrt{2g(h_1(t) - h_2(t))}$$

$$f_{wy2}(t) = A_{w2} \sqrt{2gh_2(t)}$$

$$\begin{cases} A_1 \dot{h}_1(t) = f_{we}(t) - A_{w1} \sqrt{2g(h_1(t) - h_2(t))} \\ A_2 \dot{h}_2(t) = A_{w1} \sqrt{2g(h_1(t) - h_2(t))} - A_{w2} \sqrt{2gh_2(t)} \end{cases}$$

---


$$\begin{cases} 0 = f_{we} - A_{w1} \sqrt{2g(h_1 - h_2)} \\ 0 = A_{w1} \sqrt{2g(h_1 - h_2)} - A_{w2} \sqrt{2gh_2} \end{cases}$$

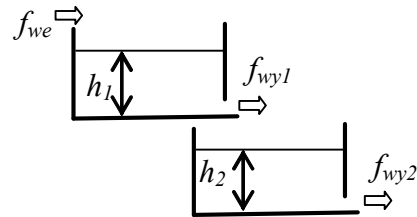
$$f_{we} = A_{w1} \sqrt{2g(h_1 - h_2)} = A_{w2} \sqrt{2gh_2}$$

$$h_1 =$$

$$h_2 =$$

# Otwarte układy hydrauliczne - linearyzacja

## Kaskada niewspółdziałająca

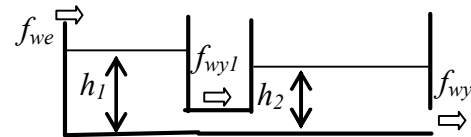


$$\begin{cases} A_1 \dot{h}_1(t) = f_{we}(t) - f_{wy1}(t) \\ A_2 \dot{h}_2(t) = f_{wy1}(t) - f_{wy2}(t) \end{cases}$$

$$f_{wy1}(t) = A_{w1} \sqrt{2gh_1(t)} \approx a_1 h_1(t)$$

$$f_{wy2}(t) = A_{w2} \sqrt{2gh_2(t)} \approx a_2 h_2(t)$$

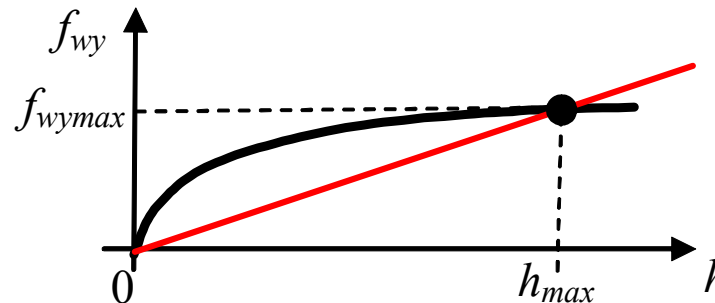
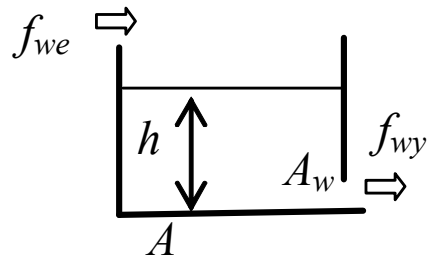
## Kaskada współdziałająca



$$\begin{cases} A_1 \dot{h}_1(t) = f_{we}(t) - f_{wy1}(t) \\ A_2 \dot{h}_2(t) = f_{wy1}(t) - f_{wy2}(t) \end{cases}$$

$$f_{wy1}(t) = A_{w1} \sqrt{2g(h_1(t) - h_2(t))} \approx a_1 (h_1(t) - h_2(t))$$

$$f_{wy2}(t) = A_{w2} \sqrt{2gh_2(t)} \approx a_2 h_2(t)$$



$$f_{wy} = A_w \sqrt{2gh} \approx ah$$

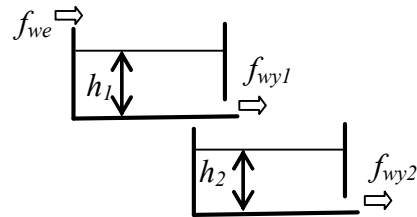
$$f_{wy_{max}} = A_w \sqrt{2gh_{max}}$$

→ a

Kiedy  $h = h_{max}$  ?

Jaką maksymalną wartość może mieć przepływ  $f_{we}$ , żeby ciecz nie wylewała się ze zbiornika?

### Kaskada niewspółdziałająca



$$\begin{cases} A_1 \dot{h}_1(t) = f_{we}(t) - a_1 h_1(t) \\ A_2 \dot{h}_2(t) = a_1 h_1(t) - a_2 h_2(t) \end{cases}$$

$$f_{we} = a_1 h_1 = a_2 h_2 \rightarrow \begin{cases} h_1 = f_{we} / a_1 \\ h_2 = f_{we} / a_2 \end{cases}$$

$$\begin{cases} (A_1 s + a_1) h_1(s) = f_{we}(s) \\ (A_2 s + a_2) h_2(s) = a_1 h_1(s) \end{cases}$$

$$\begin{cases} M_1 h_1(s) = f_{we}(s) \\ M_2 h_2(s) = a_1 h_1(s) \end{cases}$$

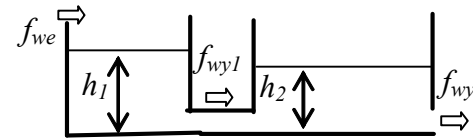
$$h_1(s) = \frac{1}{M_1} f_{we}(s)$$

$$h_2(s) = \frac{a_1}{M_1 M_2} f_{we}(s)$$

$$M_1 M_2 = (A_1 s + a_1)(A_2 s + a_2) = 0$$

$$A_1 A_2 s^2 + (A_1 a_2 + A_2 a_1) s + a_1 a_2 = 0$$

### Kaskada współdziałająca



$$\begin{cases} A_1 \dot{h}_1(t) = f_{we}(t) - a_1 (h_1(t) - h_2(t)) \\ A_2 \dot{h}_2(t) = a_1 (h_1(t) - h_2(t)) - a_2 h_2(t) \end{cases}$$

$$f_{we} = a_1 (h_1 - h_2) = a_2 h_2 \rightarrow \begin{cases} h_1 = f_{we} (a_1 + a_2) / (a_1 a_2) \\ h_2 = f_{we} / a_2 \end{cases}$$

$$\begin{cases} (A_1 s + a_1) h_1(s) = f_{we}(s) + a_1 h_2(s) \\ (A_2 s + a_1 + a_2) h_2(s) = a_1 h_1(s) \end{cases}$$

$$\begin{cases} M_1 h_1(s) = f_{we}(s) + a_1 h_2(s) \\ M_2 h_2(s) = a_1 h_1(s) \end{cases}$$

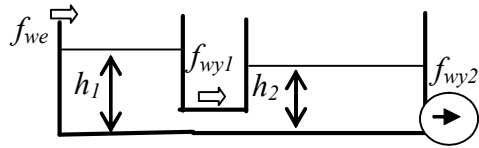
$$h_1(s) = \frac{M_2}{M_1 M_2 - a_1^2} f_{we}(s)$$

$$h_2(s) = \frac{a_1}{M_1 M_2 - a_1^2} f_{we}(s)$$

$$M_1 M_2 - a_1^2 = (A_1 s + a_1)(A_2 s + a_1 + a_2) - a_1^2 = 0$$

$$A_1 A_2 s^2 + (A_1 a_1 + A_1 a_2 + A_2 a_1) s + a_1 a_2 = 0$$

## Kaskada z pompą



$$\begin{cases} A_1 \dot{h}_1(t) = f_{we}(t) - a_1(h_1(t) - h_2(t)) \\ A_2 \dot{h}_2(t) = a_1(h_1(t) - h_2(t)) - f_{wy2}(t) \end{cases}$$

$$f_{we} = a_1(h_1 - h_2) = f_{wy2}$$

$$f_{we} = f_{wy2} \rightarrow h_1 - h_2 = f_{we} / a_1$$

$$f_{we} \neq f_{wy2} \rightarrow$$

$$\begin{cases} (A_1 s + a_1) h_1(s) = f_{we}(s) + a_1 h_2(s) \\ (A_2 s + a_1) h_2(s) = a_1 h_1(s) - f_{wy2}(s) \end{cases}$$

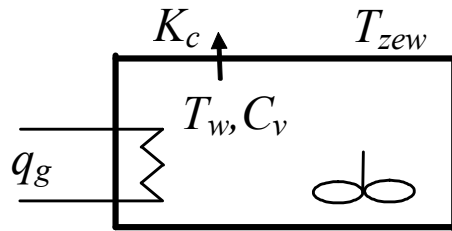
$$\begin{cases} M_1 h_1(s) = f_{we}(s) + a_1 h_2(s) \\ M_2 h_2(s) = a_1 h_1(s) - f_{wy2}(s) \end{cases}$$

$$h_1(s) = \frac{M_2}{M_1 M_2 - a_1^2} f_{we}(s) - \frac{a_1}{M_1 M_2 - a_1^2} f_{wy2}(s)$$

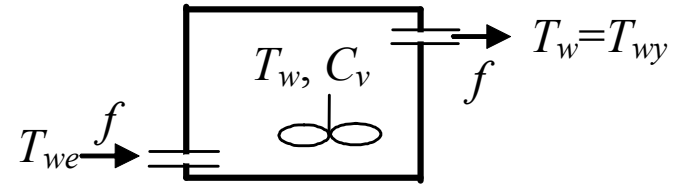
$$h_2(s) = \frac{a_1}{M_1 M_2 - a_1^2} f_{we}(s) - \frac{M_1}{M_1 M_2 - a_1^2} f_{wy2}(s)$$

$$M_1 M_2 - a_1^2 = (A_1 s + a_1)(A_2 s + a_1) - a_1^2 = s(A_1 A_2 s + A_1 a_1 + A_2 a_1) = 0$$

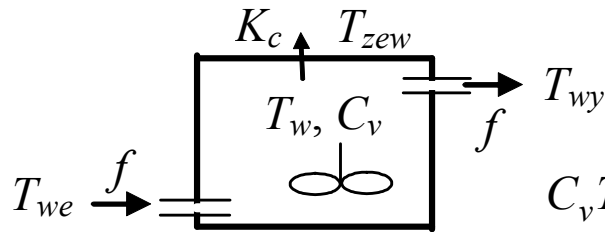
## Obiekty cieplne



$$C_v \dot{T}_w(t) = q_g(t) - K_c (T_w(t) - T_{zew}(t))$$



$$C_v \dot{T}_w(t) = c_p \rho f(t) T_{we}(t) - c_p \rho f(t) T_w(t)$$



$$C_v \dot{T}_w(t) = c_p \rho f(t) T_{we}(t) - c_p \rho f(t) T_{wy}(t) - K_c (T_w(t) - T_{zew}(t))$$

$$1) \quad T_{wy}(t) = T_w(t) \quad C_v \dot{T}_w(t) = c_p \rho f(t) T_{we}(t) - c_p \rho f(t) T_w(t) - K_c (T_w(t) - T_{zew}(t))$$

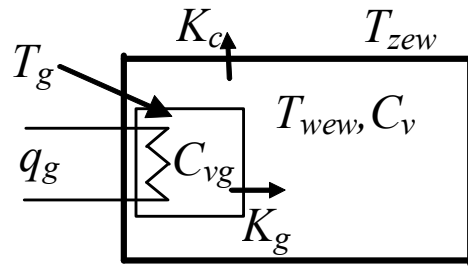
$$2) \quad T_w(t) = (T_{we}(t) + T_{wy}(t)) / 2$$

$$C_v \frac{\dot{T}_{we}(t) + \dot{T}_{wy}(t)}{2} = c_p \rho f(t) T_{we}(t) - c_p \rho f(t) T_{wy}(t) - K_c \left( \frac{T_{we}(t) + T_{wy}(t)}{2} - T_{zew}(t) \right)$$

$$3) \quad T_{wy}(t) = 2T_w(t) - T_{we}(t)$$

$$C_v \dot{T}_w(t) = c_p \rho f(t) T_{we}(t) - c_p \rho f(t) (2T_w(t) - T_{we}(t)) - K_c (T_w(t) - T_{zew}(t))$$

## Obiekty cieplne



$$\begin{cases} C_{vg} \dot{T}_g(t) = q_g(t) - K_g (T_g(t) - T_{wew}(t)) \\ C_{vw} \dot{T}_{wew}(t) = K_g (T_g(t) - T_{wew}(t)) - K_c (T_{wew}(t) - T_{zew}(t)) \end{cases}$$

wy:  $T_g, T_{wew}$

we:  $q_g, T_{zew}$

$$\begin{cases} 0 = q_g - K_g (T_g - T_{wew}) \\ 0 = K_g (T_g - T_{wew}) - K_c (T_{wew} - T_{zew}) \end{cases}$$

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$$q_g = K_g (T_g - T_{wew}) = K_c (T_{wew} - T_{zew})$$


---

$$T_{wew} = \frac{q_g}{K_c} + T_{zew}$$

$$T_g = \frac{q_g}{K_g} + T_{wew} = \frac{q_g}{K_g} + \frac{q_g}{K_c} + T_{zew}$$

Identyfikacja parametrów ( $K_g, K_c$ )

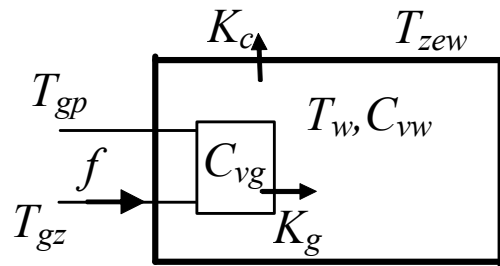
$$q_{gN}, T_{zewN}, T_{wewN}, T_{gN}$$


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$$K_c = \frac{q_{gN}}{T_{wewN} - T_{zewN}}$$

$$K_g = \frac{q_{gN}}{T_{gN} - T_{wewN}}$$

## Obiekty cieplne



$$T_{gśś}(t) = T_{gp}(t)$$

$$\begin{cases} C_{vg} \dot{T}_{gp}(t) = c_{pw} \rho_{pw} f(t) T_{gz}(t) - c_{pw} \rho_{pw} f(t) T_{gp}(t) - K_g (T_{gp}(t) - T_{wew}(t)) \\ C_{vw} \dot{T}_{wew}(t) = K_g (T_{gp}(t) - T_{wew}(t)) - K_c (T_{wew}(t) - T_{zew}(t)) \end{cases}$$

$$\begin{cases} C_{vg} \dot{T}_{gp}(t) = c_{pw} \rho_{pw} f(t) (T_{gz}(t) - T_{gp}(t)) - K_g (T_{gp}(t) - T_{wew}(t)) \\ C_{vw} \dot{T}_{wew}(t) = K_g (T_{gp}(t) - T_{wew}(t)) - K_c (T_{wew}(t) - T_{zew}(t)) \end{cases}$$

wy:  $T_{gp}, T_{wew}$

we:  $T_{gz}, T_{zew}, f$

$$\begin{cases} 0 = c_{pw} \rho_{pw} f (T_{gz} - T_{gp}) - K_g (T_{gp} - T_{wew}) \\ 0 = K_g (T_{gp} - T_{wew}) - K_c (T_{wew} - T_{zew}) \end{cases}$$

$$c_{pw} \rho_{pw} f (T_{gz} - T_{gp}) = K_g (T_{gp} - T_{wew}) = K_c (T_{wew} - T_{zew})$$

$$T_{wew} =$$

$$T_{gp} =$$

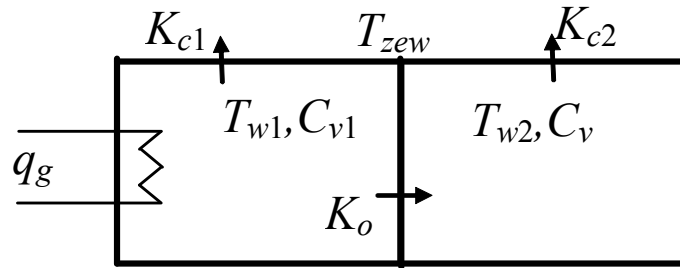
Identyfikacja parametrów ( $K_g, K_c$ )

1)  $T_{zewN}, T_{wewN}, T_{gzN}, T_{gpN}, f_N$

2)  $T_{zewN}, T_{wewN}, T_{gzN}, T_{gpN}, q_N$

$$c_{pw} \rho_{pw} f_N (T_{gzN} - T_{gpN}) = K_g (T_{gpN} - T_{wewN}) = K_c (T_{wewN} - T_{zewN}) = q_N$$

## Obiekty ciepłne



$$\begin{cases} C_{v1} \dot{T}_{w1}(t) = q_g(t) - K_{c1}(T_{w1}(t) - T_{zew}(t)) - K_o(T_{w1}(t) - T_{w2}(t)) \\ C_{v2} \dot{T}_{w2}(t) = K_o(T_{w1}(t) - T_{w2}(t)) - K_{c2}(T_{w2}(t) - T_{zew}(t)) \end{cases}$$

wy:  $T_{w1}, T_{w2}$

we:  $q_g, T_{zew}$

---


$$\begin{cases} 0 = q_g - K_{c1}(T_{w1} - T_{zew}) - K_o(T_{w1} - T_{w2}) \\ 0 = K_o(T_{w1} - T_{w2}) - K_{c2}(T_{w2} - T_{zew}) \end{cases}$$

Identyfikacja parametrów ( $K_o, K_{c1}, K_{c2}$ )

$$T_{w1} =$$

$$q_{gN}, T_{zewN}, T_{w1N}, T_{w2}$$

$$T_{w2} =$$

- 1) Konstrukcja zewnętrznych ścian jest taka sama, ale pomieszczenie 2 ma o połowę mniejszą powierzchnię ścian

$$K_{c2} = aK_{c1}, a = 0.5$$

- 2) W warunkach nominalnych pomieszczenie z grzejnikiem 60% dostarczonego ciepła traci na zewnątrz

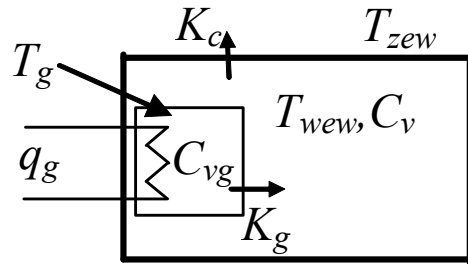
$q_g$                       dostarczane ciepło

$K_{c1}(T_{w1} - T_{zew})$       strata na zewnątrz

$K_o(T_{w1} - T_{w2})$       strata do pomieszczenia2



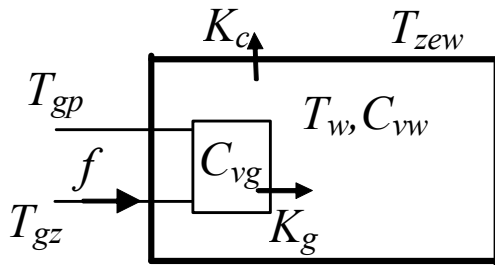
## Obiekty cieplne



$$\begin{cases} C_{vg} \dot{T}_{gp}(t) = q_g(t) - K_g (T_g(t) - T_{wew}(t)) \\ C_{vw} \dot{T}_{wew}(t) = K_g (T_g(t) - T_{wew}(t)) - K_c (T_{wew}(t) - T_{zew}(t)) \end{cases}$$

$$T_{wew}(s) = \frac{1}{M} q_g(s) + \frac{1}{M} T_{zew}(s)$$

$$T_g(s) = \frac{1}{M} q_g(s) + \frac{1}{M} T_{zew}(s)$$

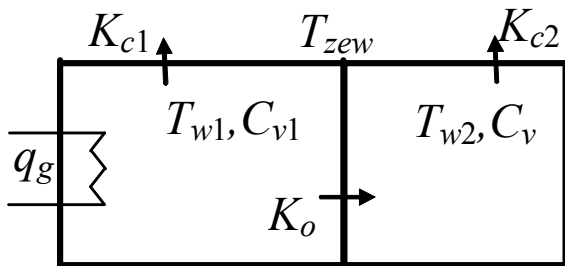


$$\begin{cases} C_{vg} \dot{T}_{gp}(t) = c_{pw} \rho_{pw} f(t) (T_{gz}(t) - T_{gp}(t)) - K_g (T_{gp}(t) - T_{wew}(t)) \\ C_{vw} \dot{T}_{wew}(t) = K_g (T_{gp}(t) - T_{wew}(t)) - K_c (T_{wew}(t) - T_{zew}(t)) \end{cases}$$

$$f(t) = \text{const}$$

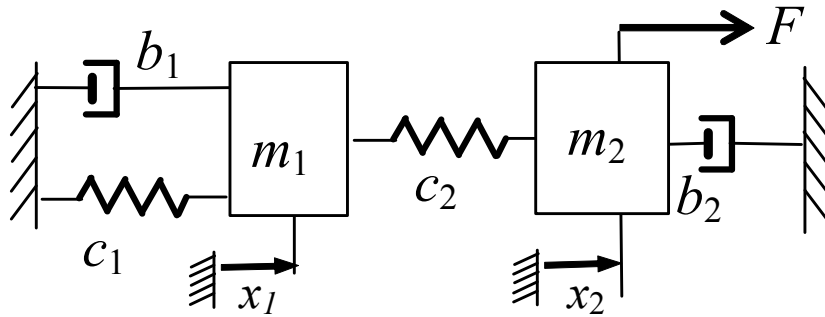
$$T_{wew}(s) = \frac{1}{M} T_{gz}(s) + \frac{1}{M} T_{zew}(s)$$

$$T_{gp}(s) = \frac{1}{M} T_{gz}(s) + \frac{1}{M} T_{zew}(s)$$

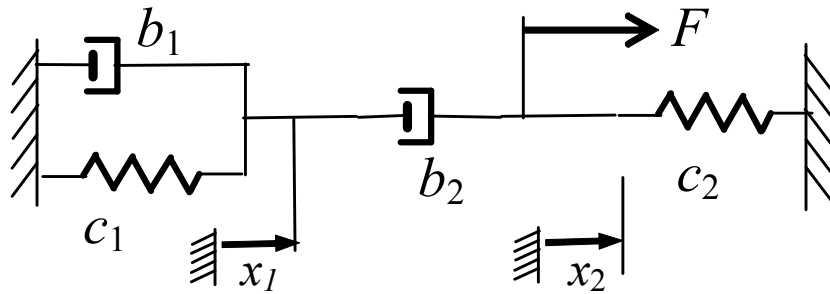


$$\begin{cases} C_{v1} \dot{T}_{w1}(t) = q_g(t) - K_{c1} (T_{w1}(t) - T_{zew}(t)) - K_o (T_{w1}(t) - T_{w2}(t)) \\ C_{v2} \dot{T}_{w2}(t) = K_o (T_{w1}(t) - T_{w2}(t)) - K_{c2} (T_{w2}(t) - T_{zew}(t)) \end{cases}$$

## Proste układy mechaniczne



$$\begin{cases} F(t) = m_2 \ddot{x}_2(t) + b_2 \dot{x}_2(t) + c_2 (x_2(t) - x_1(t)) \\ 0 = m_1 \ddot{x}_1(t) + b_1 \dot{x}_1(t) + c_1 x_1(t) + c_2 (x_1(t) - x_2(t)) \end{cases}$$



$$\begin{cases} F(t) = b_2 (\dot{x}_2(t) - \dot{x}_1(t)) + c_2 x_2(t) \\ 0 = b_2 (\dot{x}_1(t) - \dot{x}_2(t)) + c_1 x_1(t) + b_1 \dot{x}_1(t) \end{cases}$$